

## Metal piezoelectric semiconductor field effect transistors for piezoelectric strain sensors

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In this letter, we examine the potential of a functional device that can have good transistor and stress sensor properties. The device examined is based on the use of a thin oxide with high piezoelectric coefficients under the gate region. Channel charge and current are controlled by gate voltage or by stress. We examine the performance of two classes of heterostructures that are important semiconductor technologies: (i) Si/SiO<sub>2</sub>/BaTiO<sub>3</sub> heterostructure junctions that would be an important breakthrough for silicon sensor technology and (ii) GaN/AlN/BaTiO<sub>3</sub> heterostructure field effect transistors. The calculations show that with a very thin piezoelectric layer we can have a highly sensitive stress sensor and transistor. For optimum performance, the piezoelectric layer thickness should be  $\sim 30\text{--}60$  Å. © 2004 American Institute of Physics. [DOI: 10.1063/1.1784039]

In recent years, devices exploiting piezoelectric material have been developed for electromechanical actuators and sensors.<sup>1</sup> In general, piezoelectric materials are used as piezoresistive sensors. While applying bias current on the piezoresistive material, the variation of resistance induced by strain effect leads to the voltage drop. The voltage signal is then fed to the gate of field effect transistors (FETs) with high input impedance and then transduced to current by the FET. This allows us to estimate the strain by measuring the current. However, two or more devices including capacitors are needed in these detecting systems to amplify the signal, which limits the operation frequency and increases the power consumption. Furthermore, the strain measured by the piezoresistive materials is the average value cross the resistors, which is not suitable for small size detector. These considerations limit applications to microelectromechanical system.

Recently, piezoceramics grown on silicon or nitride based heterostructure junctions have attracted considerable interest.<sup>2–6</sup> For experimentalists who are working in this area, several important questions remain unanswered: (i) What are some critical physical properties that need to be measured? (ii) What kinds of devices can show performance that is superior to the existing devices? (iii) Can polar oxide-semiconductor structures create physical effects that are not possible in existing technologies? It is known that there is a strong fixed polarization charge at the heterointerface, which introduces very large electric fields and band bending, and induces a two-dimensional electron gas (2DEG) at the semiconductor heterostructure interface. For the most part, these studies have focused on the 2DEG induced by the static built in strain in the heterostructure. However, it is important to examine the response of the 2DEG to dynamic strain variations. As we know, dynamic strain leads to the change of piezoelectric polarization, which would affect the band bending and the 2DEG density. In field effect transistors (FETs), once the strain is directly applied in the FET, the variation of the 2DEG caused by strain will affect the drain-source current. Therefore we can directly measure strain through variation of drain-source current. Such a device design will have

several advantages. First, these sensors are directly embedded to FETs without the need of RC circuit, and therefore the frequency limitation would be much lower than the traditional device. The size of the FET can be submicrometer, so that the size of sensor can be extremely small. Such a power saving higher frequency FET sensor would have a great impact on sensor technology.

In this letter, we will present this theoretical model for two classes of junctions that are important for device technologies: (i) silicon based Si/SiO<sub>2</sub>/BaTiO<sub>3</sub> junctions and (ii) GaN based GaN/AlN/BaTiO<sub>3</sub> junctions. Owing to their wide band-gap, the nitride based materials are especially important for the high temperature and high voltage application. The ferroelectric material, BaTiO<sub>3</sub>, is selected due to its high piezoelectric constant<sup>7,8</sup> which is more sensitive to the variation of strain.

The formalism developed is generic and can be applied to other “smart” oxides as well. The basic structure examined by us is shown schematically in Fig. 1(a). As shown, a

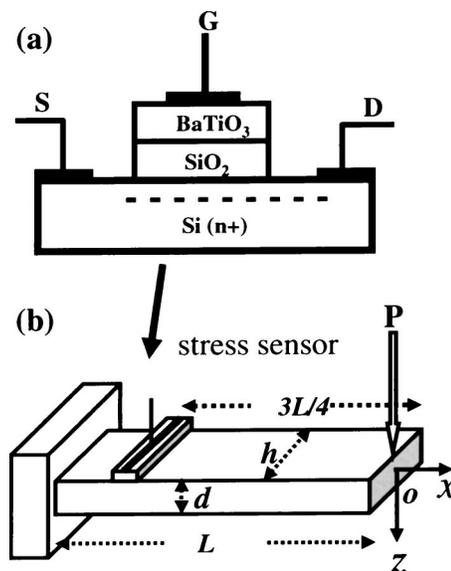


FIG. 1. (a) A schematic of the MPISFETs structure. (b) The MPISFETs is grown on top of the cantilever.

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“smart oxide” (in our simulation, this is BaTiO<sub>3</sub>) is placed between the gate and 2D channel of a FET. We note that since at present oxides such as BaTiO<sub>3</sub> are likely to have a large defect density and very poor mobility, we design the smart FET so that the free carrier density is essentially at the high quality Si/SiO<sub>2</sub> interface. The metal-piezoelectric-insulator semiconductor field effect transistor (MPISFET) sensor is assumed to be grown on silicon cantilever as shown in Fig. 1(b). When a force  $P$  applied on the side of the beam, the deflection  $\delta z$  in the  $z$  direction is given by

$$\delta z = \frac{L^3}{3EI} P, \quad (1)$$

where  $E$  is Young's modulus of the beam,  $I$  is the momentum of inertia, and  $L$  is the length of the beam. The momentum of inertia  $I$  of a rectangular beam is  $hd^3/12$ , where  $h$  is the beam width and  $d$  is the beam height. When the cantilever is under pressure, the stress  $\sigma_x$  is  $\epsilon_x E$ , where  $\epsilon_x$  is the strain and given by

$$\epsilon_x(x, -d/2) = \frac{\sigma_x(x, z)}{E} = \frac{3x(d/2)\delta z}{L^3}, \quad (2)$$

where  $z = -d/2$  since the MPISFET is grown on top of the beam. We can also derive the strain  $\epsilon_y$  is equal to  $\tau\epsilon_x$ , where  $\tau$  is the Poisson ratio. The detailed formalism can be found in Ref. 9. Here we have assumed that MPISFETs are much thinner than the height of the beam, and therefore the strain,  $\epsilon_x$  and  $\epsilon_y$ , on top of beam is equal to the strain on the piezoelectric material. For tetragonal materials such as BaTiO<sub>3</sub>,<sup>7</sup> it can be shown that the polarization in the  $z$  direction  $P_z$  is given by

$$P_z = P_{sp} + \left( e_{13} - e_{33} \frac{C_{13}}{C_{33}} \right) (\epsilon_x + \epsilon_y), \quad (3)$$

where  $e_{ij}$  is the piezoelectric constant,  $C_{ij}$  is the elastic constant, and  $P_{sp}$  is the spontaneous polarization of the piezoceramics, which is  $-0.26$  C/m<sup>2</sup> for BaTiO<sub>3</sub>. The values of  $C_{13}$  and  $C_{33}$  for BaTiO<sub>3</sub> are 211 and 160 GPa, respectively, and  $e_{31}$  and  $e_{33}$  of BaTiO<sub>3</sub> are  $-3.88$  and  $5.48$  C/m<sup>2</sup>, respectively. The dielectric constant of BaTiO<sub>3</sub> is  $48 \epsilon_0$ .<sup>7</sup> Once the polarization  $P_z$  is obtained, the two-dimensional electron gas induced by the polarization can be calculated by a charge-control model,<sup>10,11</sup> which solves the Poisson equation and Schrödinger equation self-consistently.

To study the performance of the MPISFET sensor, we first begin with Si/SiO<sub>2</sub>/BaTiO<sub>3</sub> heterostructure junctions. Traditionally, silicon is used for mechanical sensors, because it combines well-established electronic properties with excellent mechanical properties.<sup>12</sup> Therefore, the component of the cantilever is assumed to be silicon in this case. The Young's modulus and Poisson ratio for silicon is 130 GPa and 0.28, respectively.<sup>13</sup> In Fig. 2 we show how the sheet charge density in the channel changes as stress increases. In Fig. 2(a), we show the 2DEG at the BaTiO<sub>3</sub>/SiO<sub>2</sub> junction while in Fig. 2(b), it is shown at the Si/SiO<sub>2</sub> junction. We see that for a 50 and 30 Å BaTiO<sub>3</sub> film, a large part of the electron free charge resides at the BaTiO<sub>3</sub>/SiO<sub>2</sub> interface. Since it is expected that mobile charge will have very poor transport properties and may cause deleterious trap related problems, it is important that most of the electron charge resides at the Si/SiO<sub>2</sub> interface. We see that once BaTiO<sub>3</sub> thickness reaches 20 Å, the channel charge is all at the Si/SiO<sub>2</sub> inter-

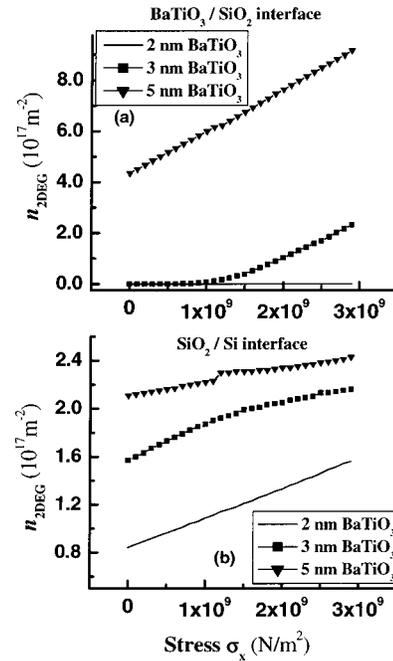


FIG. 2. Calculated sheet charge densities, ( $n_{2DEG}$ ), for the Si/SiO<sub>2</sub>/BaTiO<sub>3</sub> heterostructure junctions. (a) The  $n_{2DEG}$  at the SiO<sub>2</sub>/BaTiO<sub>3</sub> interface. (b) The  $n_{2DEG}$  at the Si/SiO<sub>2</sub> interfaces.

face and the device acts as a strained metal-oxide-semiconductor FET but with a very large stress response. We find a slope of  $dn/d\sigma_x = 2.57 \times 10^7 \text{ N}^{-1}$  for the optimal configuration. As can be seen from Fig. 2(b), a large change in channel current is expected as stress changes.

We next consider GaN/AlN/BaTiO<sub>3</sub> heterojunctions. It is known there is a large spontaneous polarization in the nitrides. Additionally, the piezoelectric effect is also very strong, which would induce large polarization under the strain condition. Therefore, nitrides would be good choice for piezoelectric sensors. The crystal structure of nitride is wurtzite. The piezoelectric polarization induced by the strain would be the same as Eq. (3). The material of cantilever is assumed to be GaN in this calculation. The elastic constants  $C_{13}$  of AlN and GaN are 100 and 110 GPa, respectively, and the  $C_{33}$  of both are 390 GPa. The piezoelectric constants  $e_{31}$  of AlN and GaN are  $-0.58$  and  $-0.34$  C/m<sup>2</sup>, respectively. The  $e_{33}$  of AlN and GaN are 1.55 and 0.67 C/m<sup>2</sup>, respectively. The piezoelectric constants of GaN and AlN are similar, which cancels part of the fixed polar charge variation at the GaN/AlN interface induced by the strain. Therefore, a structure with a thin BaTiO<sub>3</sub> layer on top is considered to improve the sensor properties. Figure 3 shows a schematic of the structure and the results for using GaN/AlN/BaTiO<sub>3</sub> heterostructure junctions. Once again a large thickness of BaTiO<sub>3</sub> layer leads to higher band bending in the BaTiO<sub>3</sub> layer and accumulation of sheet charge density at the AlN/BaTiO<sub>3</sub> interface. This would lower the performance of sensor and mobility of FETs channel. The optimal thickness of BaTiO<sub>3</sub> is 30 Å, for which the slope  $dn/d\sigma_x$  is equal to  $1.608 \times 10^7 \text{ (N}^{-1}\text{)}$ .

The parameters for oxides used in the calculations are assumed to be those for perfect bulk materials. However, in reality, the properties of thin film piezoelectric or pyroelectric material may have difference from the bulk crystal. Recently, several theoretical and experimental reports<sup>14,15</sup> indicate that the spontaneous polarization of BaTiO<sub>3</sub> would

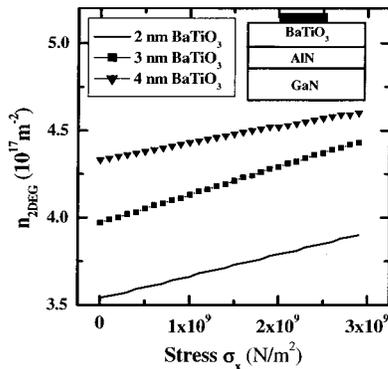


FIG. 3. Calculated sheet charge densities, ( $n_{2DEG}$ ), for the GaN/AlN heterostructure interface. The thickness of AlN layer is 30 Å.

decrease when the film thickness is smaller than 100 Å. There are reports of a critical thickness, 24 Å for BaTiO<sub>3</sub> thin layer to keep its spontaneous polarization. The spontaneous polarization decrease to  $-0.05$  C/m<sup>2</sup> at the critical thickness. In order to determine the influence caused by parameter changes, we examine the optimal thickness for different dielectric constant and spontaneous polarization. Figure 4 shows the calculated optimal BaTiO<sub>3</sub> layer thickness versus the spontaneous polarization for different dielectric constants. When the spontaneous polarization decreases to  $-0.05$  C/m<sup>2</sup>, the optimum BaTiO<sub>3</sub> changes from 30 to 60 Å. It is also clear that optimal polar material layer thickness is roughly proportional to  $1/\epsilon$ . We can see in Fig. 4 that when  $\epsilon$  is assumed to be  $200 \epsilon_0$ , we obtain an optimum layer thickness of  $\sim 85$  Å. Thus if  $\epsilon$  increases or spontaneous polarization decreases, the optimum thickness of polar materials in-

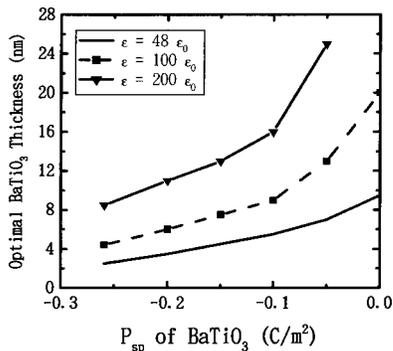


FIG. 4. Calculated optimal BaTiO<sub>3</sub> layer thickness of Si/SiO<sub>2</sub>/BaTiO<sub>3</sub> heterostructure sensor-FETs vs spontaneous polarization for different dielectric constants. The thickness of SiO<sub>2</sub> layer is 8 Å. As discussed in the text, at the optimal thickness the 2DEG is located at the SiO<sub>2</sub>/Si interface.

creases. In some references,<sup>9</sup> the  $\epsilon$  is  $1900 \epsilon_0$ , we obtain an optimum layer thickness of  $\sim 800$  Å. The parameter study of Fig. 4 would be useful for device design.

One must note that the use of polar oxides can also influence tunneling related to the gate current. The band bending will lead to higher tunneling current.<sup>16</sup> Therefore, an insulator or wide band gap (SiO<sub>2</sub> and AlN) between polar oxide and semiconductor would be necessary to stop the tunneling effect. Another aspect that needs to be further considered is the electrostatics at the heterostructure interface. Recently, some studies<sup>17</sup> indicate the band offset at oxide/Si interface can be changed. Therefore, the tunneling mechanism and optimal thickness might be affected. These effects need more experimental data to examine.

In summary, our results show that a very thin piezoelectric layer can allow a super sensitive stress sensor and a high transconductance. Besides, the size of FET sensors can be very small and thin which can be very easily integrated into electronic circuits and microprocessors. An important outcome of our study is that the thickness of the BaTiO<sub>3</sub> film is quite small (i.e., in the range of 20–50 Å). As a result, epitaxial growth technologies such as MBE are needed.

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- <sup>1</sup>A. J. Moulson and J. M. Herbert, *Electroceramics* 2nd ed. (Wiley, London, 2003).
- <sup>2</sup>Y.-Y. Lin and J. Singh, *J. Appl. Phys.* **91**, 9297 (2002).
- <sup>3</sup>B. T. Liu, K. Maki, Y. So, V. Nagarajan, R. Ramesh, J. Lettieri, J. H. Haeni, D. G. Schlom, W. Tian, X. Q. Pan, F. J. Walker, and R. A. McKee, *Appl. Phys. Lett.* **80**, 4801 (2002).
- <sup>4</sup>B. Shen, W. P. Li, T. Someya, Z. Xia Bi, J. Liu., H.-M. Zhou, R. Zhang, F. Yan, Y. Shi, Z.-G. Liu, Y.-D. Zheng, and Y. Arakawa, *Jpn. J. Appl. Phys., Part 1* **41**, 2528 (2002).
- <sup>5</sup>A. Schmehl, F. Lichtenberg, H. Bielefeldt, J. Mannhart, and D. G. Schlom, *Appl. Phys. Lett.* **82**, 3077 (2003).
- <sup>6</sup>A. P. Dmitriev, V. Y. Kachorovskii, M. S. Shur, and R. Gaska, *J. Appl. Phys.* **94**, 566 (2003).
- <sup>7</sup>Z. Li, S.-K. Chan, M. H. Grimsditch, and E. S. Zouboulis, *J. Appl. Phys.* **70**, 7327 (1991).
- <sup>8</sup>S. Saha and T. P. Sinha, *Phys. Rev. B* **62**, 8828 (2000).
- <sup>9</sup>A. J. Moulson and J. M. Herbert, in Ref. 1, Chap. 6 pp. 381–402.
- <sup>10</sup>M. Singh, J. Singh, and U. Mishra, *J. Appl. Phys.* **91**, 2989 (2002).
- <sup>11</sup>M. Singh, Y. Zhang, J. Singh, and U. Mishra, *Appl. Phys. Lett.* **77**, 1867 (2000).
- <sup>12</sup>K. E. Peterson, *Proc. IEEE* **70**, 420 (1992).
- <sup>13</sup>E. Anastassakis and M. Siakavellas, *J. Appl. Phys.* **90**, 144 (2001).
- <sup>14</sup>J. Junquera and P. Ghosez, *Nature (London)* **422**, 506 (2003).
- <sup>15</sup>M. G. Stachiotti, *Appl. Phys. Lett.* **84**, 251 (2004).
- <sup>16</sup>Y.-R. Wu, M. Singh, and J. Singh, *J. Appl. Phys.* **94**, 5826 (2003).
- <sup>17</sup>R. A. Mckee, F. J. Walker, B. Nardelli, W. A. Shelton, and G. M. Stocks, *Science* **300**, 1726 (2003).